Copyright © 1984, by the author(s). All rights reserved.

Permission to make digital or hard copies of all or part of this work for personal or classroom use is granted without fee provided that copies are not made or distributed for profit or commercial advantage and that copies bear this notice and the full citation on the first page. To copy otherwise, to republish, to post on servers or to redistribute to lists, requires prior specific permission.

ROBUST STABILITY UNDER ADDITIVE PERTURBATIONS

bу

A. Bhaya and C. A. Desoer

Memorandum No. UCB/ERL M84/110

7 December 1984

ROBUST STABILITY UNDER ADDITIVE PERTURBATIONS

by

A. Bhaya and C. A. Desoer

Memorandum No. UCB/ERL M84/110
7 December 1984

ELECTRONICS RESEARCH LABORATORY

College of Engineering University of California, Berkeley 94720

Robust Stability Under Additive Perturbations

A. Bhaya and C. A. Desoer

Department of Electrical Engineering and Computer Sciences and the Electronics Research Laboratory University of California, Berkeley, CA 94720

Abstract

We consider a MIMO linear time-invariant feedback system ${}^1S(P,C)$ which is assumed to be \mathscr{U} -stable. The plant P is subjected to an additive perturbation ΔP which is <u>proper</u> but <u>not necessarily stable</u>. We prove that the perturbed system is \mathscr{U} -stable if and only if $\Delta P[I+Q\cdot\Delta P]^{-1}$ is \mathscr{U} -stable. (Here $Q:=C(I+PC)^{-1}$.)

Professor C. A. Desoer
Department of Electrical Engineering
and Computer Sciences
University of California
Berkeley, CA 94720

(415) 642-0459 (415) 642-8458

I. Introduction

One of the main purposes of feedback is to reduce the sensitivity of the closed-loop system to changes in the plant, and it is very important to determine whether a feedback system remains stable after being subjected to changes in the plant. There is an abundant literature on this subject with various restrictions imposed on the nature of i) the plant (linear lumped [Des. 1], [Åst. 1], [Fra. 1] [Doy. 1]; linear distributed [Chen 1], [Chen 2]; nonlinear and time-varying [Zam. 1], [San. 1]), ii) the perturbation (stable [Åst. 1], [Fra. 1], [Cru. 1] [Pos. 1], [Zam. 2]) - all giving only sufficient conditions; a class of possibly unstable perturbations [Doy. 1], [Chen 1] with necessary and sufficient conditions (n.a.s.c.); fractional perturbations [Chen 2] which gave n.a.s.c.

In this note we consider exclusively MIMO linear time-invariant systems, we state and give a simple algebraic proof of a <u>necessary and sufficient condition for \mathcal{U} -stability (\mathcal{U} refers to an undesirable symmetric region of the complex plane (\mathfrak{L}_+) of the feedback system $^1S(P,C)$ (Fig. 1, solid lines) under <u>arbitrary</u> perturbations ΔP (i.e. ΔP is <u>not</u> required to be \mathcal{U} -stable). In Section II we formalize the following intuitive argument: a) the addition of ΔP to $^1S(P,C)$ (as shown by dotted lines in Fig. 1) creates a new loop; b) the "gain seen by ΔP ," through $^1S(P,C)$ is equal to $-Q:=-C(I+PC)^{-1}$; c) since the nominal system $^1S(P,C)$ is \mathcal{U} -stable, Q is \mathcal{U} -stable, d) view the new loop as $^1S(Q,\Delta P)$ as shown in Fig. 2: it is \mathcal{U} -stable $\underbrace{iff}_{\Delta P} (I+Q\cdot\Delta P)^{-1}:=Q_1$ is \mathcal{U} -stable by the Q-parametrization theorem [Zam. 2], [Des. 2]. If, in addition, ΔP is \mathcal{U} -stable, the new loop is stable $\underbrace{iff}_{\Delta P}$ det $[I+Q\cdot\Delta P](s) \neq 0$, $\forall s \in \mathcal{U}$; e) $\widetilde{S}(P,\Delta P,C)$ is \mathcal{U} -stable $\underbrace{iff}_{\Delta P}$ the new loop is \mathcal{U} -stable. These statements are intuitively</u>

appealing, however it is not clear whether some particular restrictions on P, C, ΔP are required to make them true. We prove that they hold even if P, C and ΔP are unstable!

II. Statement and Proof of Theorem

<u>Definition</u>: $\tilde{S}(P,\Delta P,C)$ (defined in Fig. 1) is $\underline{\mathcal{U}\text{-stable}}$ iff $H_{vu}: (u_1,u_2,u_3) \mapsto (y_1,y_2,y_3)$ is $\mathcal{U}\text{-stable}$.

Assumptions:

Al.
$$P(s) \in \mathbb{R}_p(s)^{n_0 \times n_1}$$
, $C(s) \in \mathbb{R}_p(s)^{n_1 \times n_0}$, $det[I+PC](\infty) \neq 0$.

A2. All hidden modes of P and C are U-stable.

A3.
$$\Delta P \in \mathbb{R}_{D}(s)^{n_0 \times n_1}$$
 and $det[I+(P+\Delta P)C](\infty) \neq 0$.

<u>Comment:</u> Note that P, C, ΔP are only required to be <u>proper</u> but <u>may be</u> <u>unstable</u>. Of course the nominal and perturbed systems are required to be well-posed (see Al and A3).

Theorem: Let A1, A2 and A3 hold. If ${}^{1}S(P,C)$ is \mathscr{U} -stable, then

- a) $\tilde{S}(P,\Delta P,C)$ is \mathscr{U} -stable $\iff \Delta P \cdot (I+Q\cdot\Delta P)^{-1}$ is \mathscr{U} -stable;
- b) $\tilde{S}(P,\Delta P,C)$ is \mathscr{U} -stable \Leftrightarrow $\tilde{S}(Q,\Delta P)$ is \mathscr{U} -stable.

If, in addition, ΔP is 2c-stable, then

c) $\tilde{S}(P,\Delta P,C)$ is \mathcal{U} -stable \Leftrightarrow det $[I+Q\cdot\Delta P](s) \neq 0$, $\forall s \in \mathcal{U}$.

<u>Comments</u>: a) Define $H_{eu}: (u_1, u_2, u_3) \mapsto (e_1, e_2, e_3)$. By writing the relation between the e_i 's, u_i 's and y_i 's it is easy to check that H_{yu} is \mathcal{U} -stable implies that H_{eu} is \mathcal{U} -stable. We will prove H_{vu} is \mathcal{U} -stable.

b) Suppose $\Delta P = R/(s-p)$ where $R \in \mathbb{C}^{n\times n}$ and p may be in \mathcal{U} . It is easy to check that $\Delta P(I+Q\Delta P)^{-1}=R[(s-p)I+QR]^{-1}$. Since the expression in brackets is analytic in \mathcal{U} , by part c) of the theorem, we have:

 $\tilde{S}(P,\Delta P,C)$ is \mathscr{U} -stable \iff det $[(s-p)I+Q(s)R] \neq 0$, $\forall s \in \mathscr{U}$ In some applications, [Bha. 1], R turns out to be a dyad, say cb^T (with b, $c \in \mathbb{C}^n$): hence, the n.a.s.c. condition for \mathscr{U} -stability reduces to a scalar condition:

$$(s-p) + b^{\mathsf{T}}Q(s)c \neq 0 \quad \forall s \in \mathcal{U}.$$

<u>Proof</u>: The summing node equations for $\tilde{S}(P,\Delta P,C)$ are:

$$e_2 - Ce_1 = u_2$$
 (1)

$$Pe_2 + e_1 + \Delta Pe_3 = u_1$$
 (2)

$$- Ce_1 + e_3 = u_3$$
 (3)

Apply the following block elementary row operations $\rho_2 + \rho_2 - P\rho_1$ and then $\rho_3 + \rho_3 + Q\rho_2$ and note that w.l.o.g. we can set $u_1 = u_2 = 0$, thus obtaining:

$$\begin{bmatrix} I & -C & 0 \\ 0 & I+PC & \Delta P \\ 0 & 0 & I+Q\Delta P \end{bmatrix} \begin{bmatrix} e_2 \\ e_1 \\ e_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ u_3 \end{bmatrix}$$

Using back-substitution and Fig. 1, we obtain:

$$y_3 = \Delta P \cdot e_3 = \Delta P (I + Q \Delta P)^{-1} u_3$$
 (4)

$$y_1 = Ce_1 = -C(I+PC)^{-1}\Delta Pe_3 = -Qy_3$$
 (5)

$$y_2 = Pe_2 = PCe_1 = -PQy_3$$
 (6)

Pf. of a) (\Rightarrow) By assumption $\tilde{S}(P,\Delta P,C)$ is \mathscr{U} -stable, hence by (4) $\Delta P(I+Q\Delta P)^{-1}$ is \mathscr{U} -stable.

- (\Leftarrow) By assumption, ${}^1S(P,C)$ is $\mathscr U$ -stable, hence Q and PQ are $\mathscr U$ -stable. Also, by assumption, $\Delta P(I+Q\Delta P)^{-1}$ is $\mathscr U$ -stable. Hence (4)-(6) show that H_{VU} is $\mathscr U$ -stable.
- <u>Pf. of b</u>). Note that because Q is known to be \mathcal{U} -stable, ${}^{1}S(Q,\Delta P)$ is \mathcal{U} -stable <u>iff</u> $\Delta P(I+Q\Delta P)^{-1}$ is \mathcal{U} -stable by the Q-parametrization theorem [Zam. 2], [Des. 2].
- Pf. of c). By assumption ${}^1S(P,C)$ is \mathscr{U} -stable; Q and ΔP are also \mathscr{U} -stable. Since \mathscr{U} -stable matrices form a ring, $(I+Q\Delta P)^{-1}$ is \mathscr{U} -stable \Leftrightarrow det $[I+Q\Delta P](s) \neq 0$, $\forall s \in \mathscr{U}$.

<u>Comments</u>: Since the proof is purely algebraic, Assumption Al is not strictly necessary - the theorem holds for linear distributed plants either continuous-time or discrete-time by working in the appropriate algebra (see, for example [Des. 3]).

References

- [Åst. 1] K. J. Åstrom, "Robustness of a design method based on assignment of poles and zeros," <u>IEEE Trans. Automat. Contr.</u>, Vol. AC-25, pp. 588-591, June 1980.
- [Bha. 1] A. Bhaya and C. A. Desoer, "On the design of large flexible space structures," submitted to <u>IEEE Trans. on Automat. Contr.</u>
- [Chen 1] M. J. Chen and C. A. Desoer, "Necessary and sufficient condition for robust stability of linear distributed feedback systems," Int. J. Contr., Vol. 35, pp. 255-267, Feb. 1982.
- [Chen 2] M. J. Chen and C. A. Desoer, "Algebraic theory for robust stability of interconnected systems: necessary and sufficient conditions," <u>IEEE Trans. Automat. Contr.</u>, Vol. AC-29, No. 6, pp. 511-519, June 1984.
- [Cru. 1] J. B. Cruz., Jr., J. S. Freudenberg, and D. P. Looze, "A relationship between sensitivity and stability of multivariable feedback systems, <u>IEEE Trans. Automat</u>, <u>Contr.</u>, Vol. AC-26, pp. 66-74, Feb. 1981.
- [Des. 1] C. A. Desoer, F. M. Callier, and W. S. Chan, "Robustness of stability conditions for linear time-invariant feedback systems,"

 IEEE Trans. Automat. Contr., Vol. AC-22, pp. 586-590, Aug. 1977.
- [Des. 2] C. A. Desoer and M. J. Chen, "Design of multivariable feedback systems with stable plant," <u>IEEE Trans. Automat. Contr.</u>, Vol. AC-26, No. 2, pp. 408-415, April 1981.
- [Des. 3] C. A. Desoer and C. L. Gustafson, "Algebraic theory of linear multivariable feedback systems," <u>IEEE Trans. Automat. Contr.</u>, vol. AC-29, No. 10, pp. 909-916, Oct. 1984.

- [Doy. 1] J. C. Doyle and G. Stein, "Multivariable feedback design:

 concepts for a classical/modern synthesis," <u>IEEE Trans. Automat.</u>

 <u>Contr.</u>, Vol. AC-26, pp. 4-16, Feb. 1981.
- [Fra. 1] B. A. Francis, "On robustness of the stability of feedback systems," IEEE Trans. Automat. Contr., Vol. AC-25, pp. 817-818, Aug. 1980.
- [Pos. 1] I. Postlethwaite, J. M. Edmunds, and A. G. MacFarlane, "Principal gains and principal phases in the analysis of linear multivariable feedback systems," <u>IEEE Trans. Automat. Contr.</u>, Vol. AC-26, pp. 32-46, Feb. 1981.
- [San. 1] N. R. Sandell, Jr. "Robust stability of systems with applications to singular perturbations," <u>Automatica</u>, Vol. 15, pp. 467-470, 1979.
- [Zam. 1] G. Zames, "Nonlinear operators for systems analysis," Res. Lab. Electron., M.I.T., Cambridge, MA, Tech. Rep. 370, Aug. 1960 (especially pp. 34-37; the derivation is based on the small gain theorem).
- [Zam 2] G. Zames, "Feedback and optimal sensitivity: Model reference transformations, multiplicative seminorms, and approximate inverses," <u>IEEE Trans. Automat. Contr.</u> Vol. AC-26, pp. 301-320, April 1981.

Figure Captions

- Fig. 1. The figure shows the system $\tilde{S}(P,\Delta P,C)$ with inputs u_1 , u_2 , u_3 and outputs y_1 , y_2 , y_3 . If the dotted part of the diagram is removed, we are left with ${}^1S(P,C)$ whose inputs are u_1 , u_2 and outputs y_1 , y_2 .
- Fig. 2. ${}^1S(Q,\Delta P)$ obtained from Fig. 1. The "gain seen by ΔP ," going from point a to point b through ${}^1S(P,C)$, is equal to -Q.

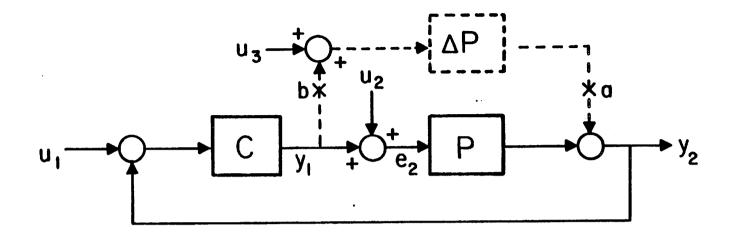


Fig. 1

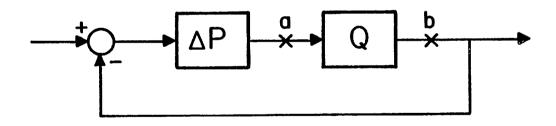


Fig. 2